

**Buck converter operated in CCM**

Christophe Basso - Switch Mode Power Supplies: SPICE Simulations and Practical Designs  
Second Edition - January 2014

**1) Input data**

$$D := 0.3338 \quad L_1 := 10 \mu\text{H} \quad T_{sw} := 4 \mu\text{s} \quad V_{in} := 15 \text{ V} \quad R_{load} := 0.5 \Omega$$

**2) Calculations**

$$V_{out} := D \cdot V_{in} = 5.007 \text{ V} \quad I_{out} := \frac{V_{out}}{R_{load}} = 10.014 \text{ A} \quad F_{sw} := \frac{1}{T_{sw}} = 250 \text{ kHz} \quad M := \frac{V_{out}}{V_{in}} = 0.334$$

Beyond this load value, the converter operates in DCM:  $R_{crit} := 2 \cdot L_1 \cdot F_{sw} \cdot \left( \frac{V_{in}}{V_{in} - V_{out}} \right) = 7.505 \Omega$

$$\Delta I_L := \frac{V_{in} - V_{out}}{L_1} \cdot D \cdot T_{sw} = 1.334 \text{ A}$$

$$I_p := I_{out} + \frac{\Delta I_L}{2} = 10.681 \text{ A}$$

$$I_V := I_{out} - \frac{\Delta I_L}{2} = 9.347 \text{ A}$$

$$\tau_L := \frac{L_1}{R_{load} \cdot T_{sw}} = 5$$

**2.1) Inductor rms current**

$$I_{L1} := \frac{\sqrt{I_V^2 + I_V \cdot I_p + I_p^2}}{\sqrt{3}} = 10.021 \text{ A}$$

$$\frac{\sqrt{12 \cdot I_{out}^2 + \Delta I_L^2}}{2 \cdot \sqrt{3}} = 10.021 \text{ A}$$

$$I_{out} \cdot \sqrt{1 + \frac{(1-D)^2 \cdot R_{load}^2}{12 \cdot F_{sw}^2 \cdot L_1^2}} = 10.021 \text{ A}$$

$$\frac{V_{out}}{R_{load}} \cdot \sqrt{1 + \frac{1}{12} \cdot \left( \frac{1-D}{\tau_L} \right)^2} = 10.021 \text{ A}$$

**2.2) Switch rms current**

$$I_{SW} := \sqrt{\frac{D \cdot (I_V^2 + I_V \cdot I_p + I_p^2)}{3}} = 5.79 \text{ A}$$

$$\frac{\sqrt{D \cdot (12 \cdot I_{out}^2 + \Delta I_L^2)}}{2 \cdot \sqrt{3}} = 5.79 \text{ A}$$

$$I_{out} \cdot \sqrt{D + \frac{D \cdot (1-D)^2 \cdot R_{load}^2}{12 \cdot F_{sw}^2 \cdot L_1^2}} = 5.79 \text{ A}$$

$$\frac{V_{out}}{R_{load}} \cdot \sqrt{D \cdot \left( 1 + \frac{1}{12} \cdot \left( \frac{1-D}{\tau_L} \right)^2 \right)} = 5.79 \text{ A}$$

**2.3) Diode rms current**

$$I_{DIODE} := \sqrt{\frac{(1-D) \cdot (I_V^2 + I_V \cdot I_p + I_p^2)}{3}} = 8.18 \text{ A}$$

$$\frac{\sqrt{(12 \cdot I_{out}^2 + \Delta I_L^2) \cdot (1-D)}}{2 \cdot \sqrt{3}} = 8.18 \text{ A}$$

$$I_{out} \cdot \sqrt{1-D + \frac{(1-D)^3 \cdot R_{load}^2}{12 \cdot F_{sw}^2 \cdot L_1^2}} = 8.18 \text{ A}$$

$$\frac{V_{out}}{R_{load}} \cdot \sqrt{(1-D) \cdot \left(1 + \frac{1}{12} \cdot \left(\frac{1-D}{\tau_L}\right)^2\right)} = 8.18 \text{ A}$$

#### **2.4) Output Capacitor rms current**

$$I_{Cout} := \sqrt{\frac{12 \cdot I_{out}^2 + \Delta I_L^2}{12}} - I_{out}^2$$

$$\frac{\Delta I_L}{2 \cdot \sqrt{3}} = 0.385 \text{ A}$$

$$I_{out} \cdot \sqrt{\frac{(1-D)^2 \cdot R_{load}^2}{12 \cdot F_{sw}^2 \cdot L_1^2}} = 0.385 \text{ A}$$

$$\frac{V_{out}}{R_{load}} \cdot \left(\frac{1-D}{\sqrt{12} \cdot \tau_L}\right) = 0.385 \text{ A}$$

#### **2.5) Input Capacitor rms current**

$$I_{Cin} := \sqrt{I_{SW}^2 - (M \cdot I_{out})^2} = 4.728 \text{ A}$$